

Load Switch Thermal Considerations

Adam Hoover

Drivers and Load Switches

ABSTRACT

For nearly every integrated circuit, there are layout recommendations to ensure optimal performance. For example, high speed data lines should have matched lengths to prevent skew and DC/DC converters should have minimal parasitics to prevent spiking. When it comes to load switches, which often carry large amounts of current, the PCB can act like a heat sink, and the layout is critical to the board's ability to dissipate heat away from the device. This application report will cover:

- · Why, Where, and How Power is Dissipated in a Load Switch
- How to Manage Power Dissipated in a Load Switch
- Designing a PCB for Optimal Power Dissipation

Contents

1	Power	Power Dissipation in a Load Switch		
	1.1	Calculating Load Switch Power Dissipation	2	
	1.2	Power is Dissipated as Heat	3	
2	Managing Load Switch Power Dissipation			
	2.1	Use a Lower ON Resistance to Dissipate Less Power	3	
	2.2	Select Packaging with Sufficient Thermal Resistance	4	
	2.3	Minimize the Thermal Resistance of the PCB	2	
3	Using	Using the PCB Thermal Calculator for Load Switch Design		
	3.1	Calculating Power Dissipation for a Dual Channel Load Switch	8	
	3.2	Converting Measured Case Temperature to Junction Temperature	8	
	3.3	Using the PCB Thermal Calculator to Estimate Operating Junction Temperature	8	
4	Refere	ences	9	
		1 to a set with a second		
		List of Figures		
1	Power	r Dissipation in a Load Switch	2	
2	Effect	t of Thermal Resistance on Maximum Power Dissipation		
3	Effect of ON Resistance on Power Dissipation			
4	Simplified Model of Heat Flow for a Device with Exposed Thermal Pad			
5	PCB Bottom View of Heat Flow Cross-Section Area			
6	Simplified Model Showing the Length in Direction of Heat Flow			
7	TPS22966EVM PCB Thermal Calculator Entry		8	
8	TPS22	TPS22966EVM PCB Thermal Calculator Results		
		List of Tables		
1	Therm	nal Resistance Factors	6	
2	TPS22	2966 PCB Thermal Comparison	7	



1 Power Dissipation in a Load Switch

Load switches are commonly used to deliver large amounts of power, and being resistive in nature, they will always dissipate a fraction of that power. This section will discuss in more detail why and how load switches dissipate power.

1.1 Calculating Load Switch Power Dissipation

Even when a switch is fully on, there is still some minimal resistance. This "ON Resistance", comprised of the pass-FET element as well as pin and packaging resistances, typically accounts for most of the power dissipated in a load switch. The Power Dissipated (P_D) across this ON Resistance (R_{ON}) is a function of the Load Current (I_{LOAD}) and can be found using Equation 1:

$$P_{D} = I_{LOAD}^{2} \times R_{ON}$$
 (1)

Figure 1 illustrates how a larger load current will exponentially increase the amount of power dissipated in a load switch in relation to the ON Resistance (R_{ON}).

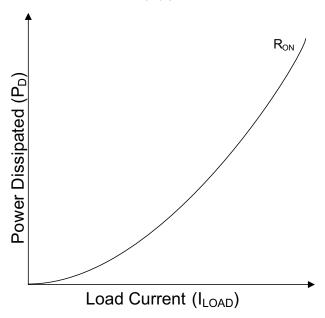


Figure 1. Power Dissipation in a Load Switch



1.2 Power is Dissipated as Heat

In accordance with the law of conservation of energy, when power is dissipated in a load switch, it has to go somewhere. In actually, it is transformed into heat energy which is then transferred from the silicon die (also known as the junction) to the device packaging, the printed circuit board, and into the air. Each of these materials will have a unique thermal resistance, which is a heat property that describes how a material will resist heat flow. The combined effectiveness of all materials to dissipate heat away from the junction is known as the Junction to Ambient Thermal Resistance or θ_{JA} .

As is the case with every integrated circuit, the junction inherently has a maximum temperature it can withstand without breaking down. This means the maximum power that can be dissipated in a load switch really becomes a question of how well heat can be transferred away from the junction. Equation 2 describes the total power ($P_{D,MAX}$) that can be dissipated in a load switch based upon the maximum operating Junction Temperature ($T_{J,MAX}$), the Ambient Air Temperature (T_A), and the Thermal Resistance from the junction to the ambient air (θ_{JA}).

$$P_{D,MAX} = \frac{T_{J,MAX} - T_A}{\theta_{JA}} \tag{2}$$

For a particular piece of end equipment, the ambient temperature range is generally fixed just like the maximum junction temperature for a particular device will be fixed. Figure 2 shows the effect a larger thermal resistance has on the maximum allowable power dissipation in a load switch with a fixed ambient and maximum junction temperature.

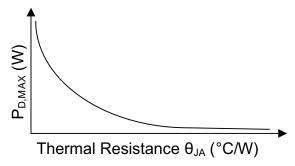


Figure 2. Effect of Thermal Resistance on Maximum Power Dissipation

2 Managing Load Switch Power Dissipation

When designing a load switch into a system, it is important to make sure the junction temperature will not exceed what is recommended in the device datasheet. This can be particularly challenging in situations where a large amount of power or heat is being dissipated inside the device. There are several methods that can be used to manage load switch power dissipation.

2.1 Use a Lower ON Resistance to Dissipate Less Power

The first method for managing power dissipation in a load switch is to simply dissipate less power to begin with. Going back to Equation 1, the power dissipated in a load switch is directly proportional to the ON Resistance. Figure 3 illustrates how a larger ON Resistance (R_{ON}) will increase the power dissipated for a given load current where $R_{ON,3} > R_{ON,2} > R_{ON,1}$.



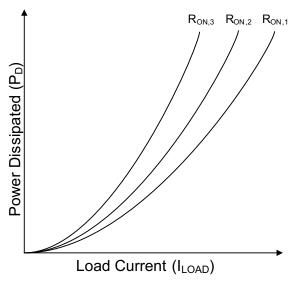


Figure 3. Effect of ON Resistance on Power Dissipation

This can be leveraged in situations with high ambient temperatures or where a large amount of current is passing through the load switch. In both cases, a lower ON Resistance will help ensure the device does exceed the maximum junction temperature rating.

2.2 Select Packaging with Sufficient Thermal Resistance

Aside from reducing the amount of power that will be dissipated as heat inside the load switch, the next best option for managing load switch power dissipation is to lower the junction to ambient thermal resistance (θ_{JA}). This begins with the device packaging. There are several different types of packages available for load switches, and the thermal properties of the package type play a key role in how the device is able to dissipate heat.

While some of the heat is radiated from the package, the majority is dissipated through convection into the air or conduction to the PCB. For packages with a large area of direct contact with the PCB, conduction can drastically increase the amount of heat that can be transferred away from the load switch. For example, a Ball Grid Array (BGA) package only makes contact through solder balls so the heat transfer path from the package to the PCB is minimal whereas a package with an exposed thermal pad has a large thermally conductive surface through which heat can be transferred.

Selecting a device based upon the packaging thermal resistance will become even more important in applications where high power dissipation or high ambient temperature is present. In general, a larger package will allow more heat to be dissipated because there is more surface area; however, this is highly dependent upon the package material and the size of the silicon die.

2.3 Minimize the Thermal Resistance of the PCB

As mentioned in the previous section, for devices with a large area of direct contact with the PCB, heat conduction into the board can drastically reduce the overall thermal resistance. This is especially true for devices with an exposed thermal pad; however, due to the complexity of the Expanded Thermal Resistance Model for a Typical PCB it is difficult to exactly predict what the thermal resistance of the board will be without modeling software (see SNVA419 for more details). There are many factors that can affect the thermal resistance of a PCB including the board area, number and size of thermal vias, number of layers, copper thickness, breaks in the copper layers, and other heat sources that might be present.

Because PCB design can change drastically, a series of JEDEC standards were developed that specify the PCB size and layout. These clearly defined board requirements allow for finding the overall junction to ambient thermal resistance (θ_{JA}) for packaged devices in a controlled way to provide a fair basis for comparison.



It is important to keep in mind that your board will most likely have substantial differences compared to the JEDEC standardized board used to generate the thermal resistance values found in the device datasheet. In the next section, we will discuss some tips on how to optimize your PCB design for heat dissipation.

2.3.1 Optimizing PCB Design for Load Switch Power Dissipation

In order to design a PCB with low thermal resistance, it is important to understand how heat will travel from the silicon junction through the packaging into the PCB and finally to the air. Figure 4 shows a simplified model of heat flow for a device with an exposed thermal pad. They key thing to note here is that the direction of heat flow is normal to the bottom surface of the package.

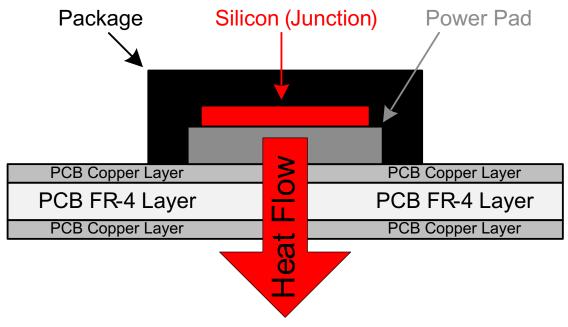


Figure 4. Simplified Model of Heat Flow for a Device with Exposed Thermal Pad

The most impactful characteristic of the PCB design is the cross-sectional area of heat flow. The cross-sectional area is linearly proportional to the PCBs ability to dissipate heat away from the device. This area is best illustrated by viewing the PCB from the bottom side as shown in Figure 5. The device position on the top side of the board is indicated with a dotted line, and the cross-sectional area with respect to direction of heat flow is colored red.

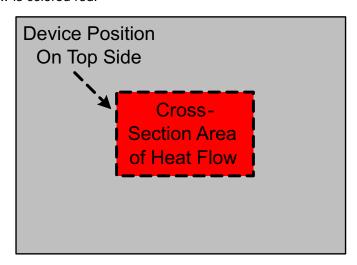


Figure 5. PCB Bottom View of Heat Flow Cross-Section Area



The next characteristic of PCB design that impacts the overall thermal resistance is the length in the direction of heat flow. The square root of the length is approximately proportional PCBs ability to dissipate heat away from the device. On a PCB, the length element would consist of the copper and FR-4 Layers as shown in Figure 6. Increasing the number of layers or the thickness of the layers will increase the overall length in the direction of heat flow and improve the board performance; however, this is generally limited by cost and manufacturing capabilities.

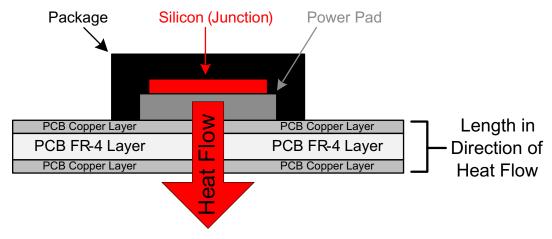


Figure 6. Simplified Model Showing the Length in Direction of Heat Flow

The next characteristic of the PCB that can be leveraged is the overall volume of the PCB. In general, a larger volume can dissipate more heat. This is often the easiest characteristic to improve because it includes the entire PCB. This could be from an increase in board area, number of copper layers, or the thickness of the copper layers. While these are also limited by manufacturing capabilities, the volumetric thermal resistance is directly related to the relative conductivity of the materials.

This leads to the fourth and final characteristic of a PCB that contributes to thermal performance which is the materials used to create the PCB. Within a certain volume, increasing the percentage of materials that conduct heat well will lower the average thermal resistance and allow the PCB to dissipate heat more effectively. Table 1 summarizes some common thermal resistance factors (R).

Material	R (m°C/W)	R (in°C/W)
Copper	0.0028	0.11
Aluminum	0.0057	0.224
FR-4	4	157
Solder 63/67	0.026	1.02
Air	36.4	1430

Table 1. Thermal Resistance Factors

Since copper has a much lower thermal resistance than FR-4, increasing the percentage of copper in the heat flow path will lower the overall thermal resistance. Therefore it is a good idea to have a copper pad under the device for direct contact whenever possible even if the packaging does not have an exposed thermal pad. Also, thermal vias should be added to the pad, and the combined area of the vias should be maximized.

2.3.2 Limited Effectiveness of Increasing the Board Area

The previous section discussed several different characteristics which can impact the thermal resistance of a PCB, but it is important to understand there is some interdependency between these characteristics. This section will show how a particular method of improving the PCB thermal performance can be limited by other board characteristics. More specifically, how increasing the PCB area is limited by the cross-sectional area, the length, and the board materials.



Table 2 compares the thermal response of the TPS22966 both on the evaluation module (EVM) and a larger test board when 6A of current are passed through each of the two channels simultaneously. The same footprint and number of vias are used in both cases, and all measurements were taken at room temperature.

TPS22966EVM TPS22966 Test Board Supply Voltage Vin = Von = Vbias = 5V Vin = Von = Vbias = 5V Inferred Image with 6A Through Each of the Two Channels Case Temp 74°C 108°C (Zone 1) PCB Edge Temp 45°C 26°C (Zone 2) PCB Area 2.25in. x 3.00in. 9.0in. × 9.0in. 2 Layers / 1oz Copper 8 Layers / 1oz Copper Layers

Table 2. TPS22966 PCB Thermal Comparison

Probably the first thing you notice is the difference in the case temperature between the two boards under the same conditions. This clearly demonstrates the impact of the PCB on the device operating temperature. Since the test board is much larger and has more layers, it can dissipate much more heat away from the device than the EVM.

Back to the main point of this section; take note of the Zone 2 temperature located near the edge of the PCBs. On the EVM, it is easy to distinguish the edge of the board because it has heated up to ~45°C. This means the entire area of the EVM board is being used to dissipate heat away from the TPS22966. The edges of the test board, on the other hand, are still at room temp ~26°C. This means only the center area of the board is actually being used to dissipate heat. This demonstrates the limited effectiveness of increasing only the board area. If more layers were added to the test board or if the copper thickness were increased, this would allow a larger area of the board to dissipate heat.

3 Using the PCB Thermal Calculator for Load Switch Design

There are a few tools available that can help when designing a PCB with a low thermal resistance. The TI PCB Thermal Calculator can provide a good estimate of the device junction temperature based upon the ambient temperature, power dissipation, and device specific thermal information.

The calculator applies only to devices with exposed thermal pads where it safe to assume a majority of the heat is dissipated through the PCB (see <u>SLUA566</u> for more details). The data presented for the TPS22966EVM in the previous section will be leveraged in this section to correlate the results of the PCB Thermal Calculator.



3.1 Calculating Power Dissipation for a Dual Channel Load Switch

In order to correlate the results of the PCB Thermal Calculator, we must first find the amount of power dissipated in the above comparison. Finding the power dissipated in a dual channel load switch is very similar to the method for finding the power dissipated in a single channel load switch as presented in Section 1.1. Basically, the total power dissipated in the device is the sum of power dissipated in each of the two channels as shown in Equation 3:

$$P_{D} = I_{LOAD, CH1}^{2} \times R_{ON, CH1}^{2} + I_{LOAD, CH2}^{2} \times R_{ON, CH2}^{2}$$
(3)

Based upon the datasheet typical characteristics graphs showing R_{ON} vs. Temperature, we can expect the ON Resistance for both channels to be approximately 20 m Ω . This can be used to find the total power dissipated in the device:

$$P_D = 6A^2 \times 20 \text{ m}\Omega + 6A^2 \times 20 \text{ m}\Omega = 1.44 \text{ Watts}$$

3.2 Converting Measured Case Temperature to Junction Temperature

The final step needed correlate the results of the PCB Thermal Calculator is to convert the case temperature found using the inferred camera to a junction temperature. Equation 4 can be used to perform this conversion using the Ψ_{JT} parameter from the device datasheet and the power dissipated found in the previous section:

$$T_{Junction} = T_{Case} + (\Psi_{JT} \times P_D)$$

$$T_{Junction} = 108^{\circ}C + (0.8^{\circ}C / W \times 1.44W)$$

$$T_{Junction} = 109.2^{\circ}C$$
(4)

3.3 Using the PCB Thermal Calculator to Estimate Operating Junction Temperature

The first step in using the thermal calculator to estimate the operating junction temperature is to select the appropriate device; in this case, the TPS22966. The 'Theta JC, Bottom' parameter is automatically filled in from the library. After entering the expected amount of power dissipation, there is an option to select either Ambient or Board Temperature conditions. For this situation, an ambient temperature of 26°C will be entered since the measurements were taken at room temperature. An example of this data entry is shown in Figure 7:

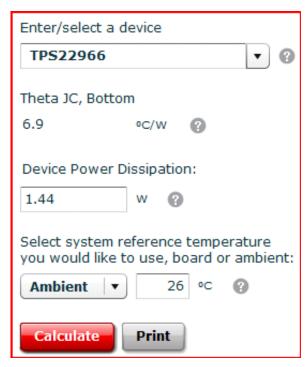


Figure 7. TPS22966EVM PCB Thermal Calculator Entry



www.ti.com References

After submitting the above information, the PCB Thermal Calculator will generate a few curves that show the expected junction and board temperatures as a function of PCB Copper Coverage Area. Although the TPS22966EVM does not have 100% copper coverage on the top side, we will use the full board area since the bottom layer has a fairly solid ground plane. The curves for this use case are shown in Figure 8.

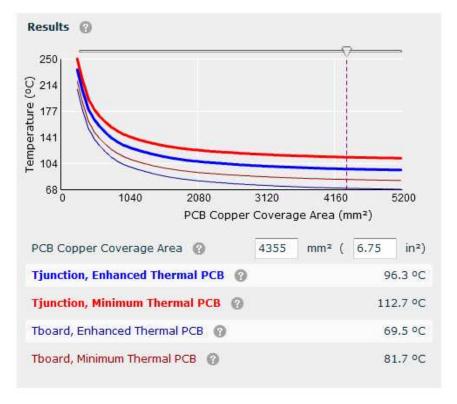


Figure 8. TPS22966EVM PCB Thermal Calculator Results

There are two curves for Tjunction and two curves for Tboard. One resents a PCB that was designed with minimal thermal characteristics, and the other represents a PCB with enhanced thermal characteristics. These serve as good bounds when estimating the operating temperature. As expected, the actual junction temperature of 109.2°C on the TPS22966EVM falls within this range.

4 References

- 1. AN-2020 Thermal Design By Insight, Not Hindsight (SNVA419)
- 2. Understanding Thermal Dissipation and Design of a Heatsink (SLVA462)
- 3. Semiconductor and IC Package Thermal Metrics application report (SPRA953)
- 4. Using Thermal Calculation Tools for Analog Components (SLUA566)
- 5. Thermal Considerations for Surface Mount Layouts (Charles Mauney, Texas Instruments)

IMPORTANT NOTICE

Texas Instruments Incorporated and its subsidiaries (TI) reserve the right to make corrections, enhancements, improvements and other changes to its semiconductor products and services per JESD46, latest issue, and to discontinue any product or service per JESD48, latest issue. Buyers should obtain the latest relevant information before placing orders and should verify that such information is current and complete. All semiconductor products (also referred to herein as "components") are sold subject to TI's terms and conditions of sale supplied at the time of order acknowledgment.

TI warrants performance of its components to the specifications applicable at the time of sale, in accordance with the warranty in TI's terms and conditions of sale of semiconductor products. Testing and other quality control techniques are used to the extent TI deems necessary to support this warranty. Except where mandated by applicable law, testing of all parameters of each component is not necessarily performed.

TI assumes no liability for applications assistance or the design of Buyers' products. Buyers are responsible for their products and applications using TI components. To minimize the risks associated with Buyers' products and applications, Buyers should provide adequate design and operating safeguards.

TI does not warrant or represent that any license, either express or implied, is granted under any patent right, copyright, mask work right, or other intellectual property right relating to any combination, machine, or process in which TI components or services are used. Information published by TI regarding third-party products or services does not constitute a license to use such products or services or a warranty or endorsement thereof. Use of such information may require a license from a third party under the patents or other intellectual property of the third party, or a license from TI under the patents or other intellectual property of TI.

Reproduction of significant portions of TI information in TI data books or data sheets is permissible only if reproduction is without alteration and is accompanied by all associated warranties, conditions, limitations, and notices. TI is not responsible or liable for such altered documentation. Information of third parties may be subject to additional restrictions.

Resale of TI components or services with statements different from or beyond the parameters stated by TI for that component or service voids all express and any implied warranties for the associated TI component or service and is an unfair and deceptive business practice. TI is not responsible or liable for any such statements.

Buyer acknowledges and agrees that it is solely responsible for compliance with all legal, regulatory and safety-related requirements concerning its products, and any use of TI components in its applications, notwithstanding any applications-related information or support that may be provided by TI. Buyer represents and agrees that it has all the necessary expertise to create and implement safeguards which anticipate dangerous consequences of failures, monitor failures and their consequences, lessen the likelihood of failures that might cause harm and take appropriate remedial actions. Buyer will fully indemnify TI and its representatives against any damages arising out of the use of any TI components in safety-critical applications.

In some cases, TI components may be promoted specifically to facilitate safety-related applications. With such components, TI's goal is to help enable customers to design and create their own end-product solutions that meet applicable functional safety standards and requirements. Nonetheless, such components are subject to these terms.

No TI components are authorized for use in FDA Class III (or similar life-critical medical equipment) unless authorized officers of the parties have executed a special agreement specifically governing such use.

Only those TI components which TI has specifically designated as military grade or "enhanced plastic" are designed and intended for use in military/aerospace applications or environments. Buyer acknowledges and agrees that any military or aerospace use of TI components which have *not* been so designated is solely at the Buyer's risk, and that Buyer is solely responsible for compliance with all legal and regulatory requirements in connection with such use.

TI has specifically designated certain components as meeting ISO/TS16949 requirements, mainly for automotive use. In any case of use of non-designated products, TI will not be responsible for any failure to meet ISO/TS16949.

Products Applications

Audio www.ti.com/audio Automotive and Transportation www.ti.com/automotive amplifier.ti.com Communications and Telecom www.ti.com/communications Amplifiers **Data Converters** dataconverter.ti.com Computers and Peripherals www.ti.com/computers **DLP® Products** www.dlp.com Consumer Electronics www.ti.com/consumer-apps DSP dsp.ti.com **Energy and Lighting** www.ti.com/energy Clocks and Timers www.ti.com/clocks Industrial www.ti.com/industrial Interface interface.ti.com Medical www.ti.com/medical Logic Security www.ti.com/security logic.ti.com

Power Mgmt power.ti.com Space, Avionics and Defense www.ti.com/space-avionics-defense

Microcontrollers microcontroller.ti.com Video and Imaging www.ti.com/video

RFID www.ti-rfid.com

OMAP Applications Processors <u>www.ti.com/omap</u> TI E2E Community <u>e2e.ti.com</u>

Wireless Connectivity <u>www.ti.com/wirelessconnectivity</u>